10 Act 20

1

Care I

TO THE MENT OF THE CONTROL OF THE SECRETARY OF THE SECRETARY CONTROL OF THE SECRETARY OF TH



UNITED STATES NAVAL ACADEMY
ENGINEERING DEPARTMENT
ANNAPOLIS, MARYLAND

Paproduced by the CLEARINGHOUSE for Federal Scientific & Technical Information Springfield Va. 22151

UNITED STATES NAVAL ACADEMY Annapolis, Maryland Engineering Department

Report E-69-3

A Commutation Formula in Continuum Mechanics

S. L. Passman *
July 1969

First Lieutenant, U. S. Army Reserve. This work was partially supported by the Naval Academy Research Council. The author gratefully acknowledges the advice of Professor C. A. Truesdell concerning Section 1.

CONTENTS

The second of th

West of the second of the seco

The second second

Total State of the State of the

A STATE OF THE STA

Stationers State S

		Pas
	INTRODUCTION	1
٥.	MATHEMATICAL PRELIMINARIES	2
1.	A COMMUTATION FORMULA	. 8
2.	GENERAL CONVECTION-DIFFUSION THEOREMS	12
	REFERENCES	16

INTRODUCTION

In a previous work [1] I have assumed the existence of a general type of convection-diffusion theorem in continuum mechanics, and have studied, the properties of this type of theorem. In this report I demonstrate that, given a tensor of any order associated with the motion of a continuum, at least one such theorem exists.

the state of the earth and the state of the state of the state of the court of the court of the state of the

O. MATHEMATICAL FRELIMINARIES

I use, essentially, the notations and assumptions of Truesdell and Toupin [2]. A short symopsis is included here in order to make this work essentially self-contained. It is emphasized that this work is formal in nature. In particular, statements concerning smoothness conditions on functions are seldom made. In general it is understood, as in formal works on differential geometry, that all functions are smooth enough to accommodate the manipulation performed and render the results meaningful. No distinction is made between a function and its values, except where confusion would result if this distinction were not made.

The results derived here are valid in Euclidean three-dimensional space. In such a space a rectangular Cartesian coordinate system always exists. We denote points in this system by the symbols Z,z. A motion is a one-parameter mapping

$$= \hat{g}(Z,t), Z = \hat{Z}(z,t), \qquad (0.1)$$

where is a real-valued parameter interpreted as the time. A point scalled a particle and a point z is called a place, or space-; sint.

We choose a single curvilinear coordinate system given by

$$x = g(z), \quad x = g(z), \quad (c.2)$$

where g is the same function in both equations. The X are called

material coordinates, and the x are called spatial coordinates.

It is convenient to use two systems of notation. The motation of general, double tensors is used when it is desired to emphasize the components of an equation. Here capital "oman" indices denote quantities which transform as tensors with respect to changes in the material coordinates X, and lower-case Roman indices denote quantities which transform as tensors with leapest to the spatial coordinates x***. The diagonal summation convention is used, and all indices have the values 1,2,3.

When display of indices would cloud the physical significance of an equation, direct notation is used.

Let are lengths at X and x be given by

AS A COME OF THE STATE OF THE ABOVE AND ASSOCIATED THE STATE OF THE STATE AND ASSOCIATED THE STATE AND ASSOCIATED THE STATE ASSOCIATED

$$ds^{2} = g_{AB} dx^{A} dx^{B} ,$$

$$ds^{2} = g_{ab} dx^{a} dx^{b} ;$$
(0.3)

gAB and gab are the components of the contravariant material and spatial metric tensors. Cristoffel symbols based on these tensors are defined in the usual manner.

Let $\mathcal{G}_{in}(x,X)$ be the components of a mixed double tensor field. The notation \mathcal{G}_{in}^{in} , denotes the covariant derivative of Φ

Double tensor fields are discussed in greater detail in [3].

^{**}This is a slight departure from the notation of [1], which uses lower-case Greek indices in this situation and upper-case Roman indices when the spatial and material coordinates are independently selected.

The exceptions are, of course, the sets of coordinates X, X^{A} ; X,

with respect to XA when the x are held constant. This derivative is called the <u>partial covariant derivative</u>, and is denoted by a comma.

$$\phi_{A,B}^{a} = \frac{\partial \phi_{A}^{a}}{\partial x^{B}} - \left\{ {}_{AB}^{C} \right\} \phi_{C}^{a} , \qquad (0.4)$$

where ∂X^B is performed with all of the x^a , and all of the X^D , $D \neq B$, held constant.

The partial covariant derivative with respect to spatial coordinates is defined in an analogous manner.

Let a one-parameter mapping between x and x be given by the composite of (0.1) and (0.2),

$$x = \hat{x}(x,t)$$
, $x = \hat{x}(x,t)$. (0.5)

The total covariant derivative of a mixed double field $\emptyset :: (x,X)$ is given by

$$\phi : ::_{A} = \phi :::_{A} + \phi :::_{A} \underbrace{ax^{a}}_{A} . \tag{C.6}$$

This derivative has the properties that when \emptyset :: is of the form $\emptyset_{C_n,D}^{A_n,B}(X)$ or $\emptyset_{C_n,d}^{a_n,b}(X)$, then \emptyset :: ; reduces to \emptyset ::; or \emptyset ::; $\frac{\partial X^e}{\partial X^c}$ respectively, and if the operation ; is performed on $\emptyset(X,X)$ then

^{*} This discussion on partial and total covariant derivatives is based on [3].

x is replaced by $\hat{x}(X,t)$, the same result is obtained as if the operation ; were performed on $\hat{x}(\hat{x}(X,t)X)$.

Let

$$\phi ::: _{;a} = \phi ::: _{,a} + \phi ::: _{,A} = \frac{\partial x^{A}}{\partial x^{a}} . \qquad (0.7)$$

If we define the Kronecker delta in the usual manner, then

$$\frac{\partial x^{a}}{\partial x^{A}} \frac{\partial x^{A}}{\partial x^{b}} = \delta^{a}_{b}, \frac{\partial x^{A}}{\partial x^{a}} \frac{\partial x^{a}}{\partial x^{B}} = \delta^{A}_{B}, \qquad (0.8)$$

and by (0.6) and (0.7)

$$\phi:::_{3A} = \phi:::_{3a} \frac{\partial x^{a}}{\partial x^{A}} , \qquad (0.9)$$

$$\mathcal{J}_{::a} = \mathcal{J}_{::A} \frac{\partial x^{A}}{\partial x^{a}} . \tag{0.10}$$

Deformation gradients are defined by

$$F_a^A = \frac{\partial x^A}{\partial x^A} = x^A, \qquad F_A^A = \frac{\partial x^A}{\partial x^A} = x^A, \qquad (0.11)$$

and composite deformation gradients are given by

$$f_{a...b}^{A...B} = f_{a}^{A} \dots f_{b}^{B}$$
, (0.12)

$$P_{A\cdots B}^{a...b} = F_{A...a}^{a} \cdot ... F_{B}^{b}$$
 (0.13)

The expansion is the absolute scalar J given by

$$J = \frac{\sqrt{\det g_{ab}}}{\sqrt{\det g_{AB}}} \det \left(\frac{\partial x^{a}}{\partial x^{A}}\right) . \tag{0.14}$$

The velocity of a particle is given by

$$\dot{x}^{a} = \frac{\partial x^{a}}{\partial t} \tag{0.15}$$

where the partial derivative is taken with X held constant.

Let $\beta(x,X,t)$ be a double tensor. The <u>material derivative</u> of ϕ is the double tensor with components

$$\frac{\mathrm{d}}{\mathrm{dt}}\mathscr{A} ::: = \frac{\partial \mathscr{A}}{\partial t} ::: + \mathscr{A} :::, \mathbf{g} \dot{\mathbf{x}}^{\mathbf{g}} . \tag{0.16}$$

where the partial time derivative is taken with both x and x held fixed, and , denotes the partial covariant derivative with respect to x. This derivative is a double tensor whose value is independent of whether x is replaced by $\hat{x}(x,t)$. It is often convenient to write $\frac{d}{dt}(x,t) = x^2 + x^2 +$

In this work, we adhere to the <u>convention</u> that <u>either the</u> <u>material or the spatial description is used</u>, <u>but not both</u>. That is, all functions are written in terms of x and t, or in terms of X and t.

It is well-known that*

$$\frac{d}{dt}(x^{a}_{A}) = \dot{x}^{a}_{A} = \dot{x}^{a}_{b} x^{b}_{A}. \qquad (0.17)$$

^{[1],§76.}

Let J be given by (0.14). Then <u>Euler's expansion formula</u>

is

$$\dot{J} = J \dot{x}^k,_k$$
 (0.18)

The acceleration is defined by

$$\ddot{\mathbf{x}}^{\mathbf{a}} = \frac{\mathbf{d}}{\mathbf{d}\mathbf{t}}(\dot{\mathbf{x}}^{\mathbf{a}}) \quad . \tag{0.19}$$

1. A COMMUTATION FORMULA

Consider a double tensor field with components $\mathscr{A}_{C...\mathfrak{p}_{C}}^{A...\mathfrak{t}_{2}}$. We have

$$p_{C...Dc,e}^{A...Ba} = \frac{3p_{C...Dc}^{A...Ba}}{3x^{e}} + \begin{cases} a \\ f \end{cases} p_{C...Dc}^{A...Bf} - \begin{cases} \epsilon \\ c \end{cases} p_{C...Dg}^{A...Bs}, \qquad (1.1)$$

so that by
$$(f',6)$$

$$\int_{C...}^{A...Ba} \frac{dx}{dx} e = \frac{\partial \mathcal{D}_{C...Dc}^{A...Ba}}{\partial x} \frac{\partial x^{e}}{\partial x^{E}} + \begin{cases} a \\ f \end{cases} e \begin{cases} A...Bf \frac{\partial x^{e}}{\partial x^{E}} \\ c...Dc \end{cases} \frac{\partial x^{e}}{\partial x^{E}}$$

$$- \begin{cases} e \\ c \end{cases} e \begin{cases} A...Ba \frac{\partial x^{e}}{\partial x^{E}} \end{cases}$$

By (0.9), (1.2) becomes

$$E_{C...De,e}^{A...Ba} = \int_{C...De;E,}^{A...Ba}$$
 (1.3)

and by the convention that only the material or the spatial description is used, but not both, we have

$$\mathcal{L}_{C...Dc.e}^{A...Ba} \times _{E}^{e} = \mathcal{L}_{C...Dc.E.}^{A...Ba}$$
(1.4)

By (1.4) and the rule is differentiating products of

By a concetation familia, (7.5) becomes

By (0.17), (1.6) becomes

$$\frac{d}{dt}(A...Ba) = A...Ba \times A...Ba \times$$

$$+ p_{C...Pc,e}^{A...Ba} \dot{x}^{e}_{,k} x^{k}_{,E}$$
 (1.7)

The last two terms in (1.7) cancel, giving

$$\frac{d}{dt}(g_{C...Dc,E}^{A...Ba}) = g_{C...Dc,e}^{A...Ba} \times^{c},_{E}$$
 (1.8)

By (1.4), (1.8) is

$$\frac{d}{dt}(p_{C...Dc,E}^{A...Ba}) = p_{C...Dc,F}^{A...Ba}; \qquad (1.9)$$

^{*[2],} p. 338.

for a tensor of the form considered $\frac{d}{dt}$ and the partial covariant derivative " $\tau_{\hat{E}}$ " commute.

In fact, the proof given above extends easily to the general case of any tensor function with any combination of covariant and contravariant, material and spatial indices. That is, for any tensor function 6 of the type considered here, "d" and ", E" compute.

$$\frac{d\mathscr{G}}{dt})_{,E} = \frac{d}{dt}(\mathscr{G}_{,E}) ,$$

$$\mathcal{G}_{AD} \mathscr{F} = \mathcal{G}_{AD} \mathscr{F} .$$

$$(1.10)$$

A formula analogous to (1.10) but containing a spatial gradient is formula. Using (1.10) and an obvious generalization of (1.4), we have

$$\left(\frac{d\mathcal{C}}{dt}\right)_{,e} \times_{\mathcal{E}} = \frac{d}{dt}\left(\mathcal{C}_{,e} \times_{,E}^{e}\right). \tag{1.11}$$

By the lamma (0.17), this becomes

$$(\frac{d\mathbf{y}}{dt})_{,e} \mathbf{x}^{e}_{,E} = \frac{d}{dt}(\mathbf{y}_{,e})\mathbf{x}^{e}_{,E} + \mathbf{y}_{,e} \mathbf{x}^{e}_{,E} , \qquad (1.12)$$

Multiplying (1.12) by X^{E} , g, using (0.8), and rearranging some indices gives

$$\frac{d}{dt}(g_{,e}) - (\frac{dg}{dt})_{,e} = -g_{,k} \dot{x}^{k}_{,e},$$

$$\frac{d}{dt}(\operatorname{grad} g) - \operatorname{grad} (\frac{dg}{dt}) = -\operatorname{grad} g \cdot \operatorname{grad} \dot{x},$$
(1.13)

which is the desired result.

The equations (1.10) and (1.13, are equivalent. It will be shown that either can be used in deriving a certain special but important type of convection-diffusion theorem.

2. GENERAL CONVECTION-DIFFUSION THEOREMS

A survey of recent developments in convection-diffusion theory and a study of the properties of a convection-diffusion theorem of a very general type have been given in [1]. In this section I demonstrate that, given a property of a particle of a continuum, with the property expressed as a tensor of a certain form, there is always a convection-diffusion theorem for that property. Furthermore, this convection-diffusion theorem is a special case of the type studied in [1].

Consider a composite deformation gradient $F_{A1...An}^{a_1...a_n}$ (no summation on n). An explicit form for its material derivative has been given in [1]. It is

$$\mathbf{\hat{F}}_{A_{1}...A_{n}}^{\mathbf{a}_{1}...a_{n}} = \sum_{i=1}^{n} \mathbf{x}_{A_{i}}^{\mathbf{a}_{i}} \mathbf{F}_{A_{1}...A_{i+1}}^{\mathbf{a}_{1}...a_{i+1}} \mathbf{A}_{i+1}...\mathbf{A}_{n}.$$
(2.1)

An easy calculation leads to

$$\dot{F}_{A_{1}...A_{n}}^{a_{1}...a_{n}} = \sum_{i=1}^{n} \dot{x}^{a_{i}}, v \quad \dot{F}_{A_{1}...A_{i-1}}^{a_{1}...a_{i-1}} \quad \dot{v} \quad \dot{a}_{i+1}...a_{n} \quad ; \qquad (2.2)$$

or

$$\dot{F}_{A_{1}\cdots A_{n}}^{a_{1}\cdots a_{n}} = \sum_{i=1}^{n-1} \dot{x}^{a_{1}} v^{a_{1}\cdots a_{i-1}} v^{a_{i+1}\cdots a_{n}} v^{a_{i+1}\cdots a_{n}} + \dot{x}^{a_{1}\cdots a_{i-1}} v^{a_{1}\cdots a_{n-1}} v^{a_{1}\cdots a_{n-1}}$$

Defining $S_{A_1...A_n}^{A_1...A_n}$ in the obvious manner, we have

$$\dot{F}_{A_{1}...A_{n}}^{a_{1}...a_{n}} = \dot{S}_{A_{1}...A_{n}}^{a_{1}...a_{n}} + \dot{x}_{n}^{a_{1}...a_{n-1}} + \dot{x}_{n-1}^{a_{1}...a_{n-1}}$$
(2.4)

Consider a tensor with covariant components $a_{a...b}$. Form the material expression $a_{a...b}$ $F_{A...B}^{a...b}$. Then

$$\frac{d}{dt}(a_{a...b} F_{A...B}^{a...b}) = \dot{a}_{a...b} F_{A...B}^{a...b} + a_{a...b} \dot{F}_{A...B}^{a...b} . \qquad (2.5)$$

Integrating along the path of a particle yields

$$a_{a...b} F_{A...B}^{a...b} = A_{A...B} + \int_{0}^{t} (\dot{a}_{a...b} F_{A...B}^{a...b} + a_{a...b} \dot{F}_{A...B}^{a...b}) dt,$$
 (2.6)

where $A_{A...B}$ is the value of $a_{a...b}$ at t=0. Using the definitions (0.12) and (0.13) and the property (0.8), we obtain from (2.2) the general convection-diffusion theorem.

$$a_{a...b} = \left[A_{A...B} + \int_{a}^{b} (\hat{a}_{c...d}^{c...d} + a_{c...d}^{c...d} + a_{c...d}^{c...d}) dt \right] f_{a...b}^{A...B} .$$
 (2.7)*

This equation states that the present value of a associated with a particular particle is the result of two processes. The first, expressed by the term

$$A_{A...B}$$
 $f_{a...b}^{A...B}$

÷ 🙀

is the shift of the initial value of a to its present position, and is independent of the intervening motion. It is called convection.

This can be further simplified by using (2.2).

The second process, expressed by the integral

$$\int_{0}^{t} (a_{c...d} F_{A...B}^{c...d} + a_{c...d} F_{A...B}^{c...d}) dt f_{a...b}^{A...B}$$

is called <u>diffusion</u>. It is seen that diffusion is a functional of the histories of a and the motion. It has been pointed out by Passman [4] that convection and diffusion are not unique processes.

The special case of (2.7) where a can be written as the spatial gradient of another tensor is of considerable interest in continuum mechanics. Let there exist a tensor b such that

$$a_{a...be} = b_{a...b,e}$$
 (2.8)

The appropriate form of (2.7) is

$$b_{a...b,e} = \begin{bmatrix} B_{A...B,E} + \int_{0}^{t} (\overline{b_{c...d,f}} F_{A...BE}^{c...df}) \\ + b_{c...d,f} \dot{F}_{A...BE}^{c...df}) dt \end{bmatrix} f_{a...be}^{A...BE} . \qquad (2.9)$$

By (1.13), this becomes

$$b_{a...b,e} = \begin{bmatrix} B_{A...B,E} + \int_{c}^{t} ([\dot{b}_{c...d,f} - b_{c...d,u} \dot{x}^{u}, f] F_{A...BE}^{c...df} \\ + b_{c...d,f} \dot{f}_{A...BE}^{c...df} \end{bmatrix} f_{a...be}^{A...BE}$$
(2.10)

Substituting (2.4) into (2.10) gives

$$b_{a...b,e} = \begin{bmatrix} B_{A...B,E} + \int_{0}^{t} (\dot{b}_{c...d,f} F_{A...EE}^{c...df} \\ + b_{c...d,f} S_{A...EE}^{c...df} \end{bmatrix} f_{a...be}^{A...EE} .$$
 (2.11)

Most of the convection-diffusion theorems familiar in continuum mechanics are consequences of (2.11).

The important relation (2.11) can be derived by an alternate method. Form the material expression $b_{a...b,E}$ $F_{A...B}^{a...b}$. By the commutation formula (1.10)

$$\frac{d}{dt}(b_{a...b,E} F_{A...B}^{a...b}) = \dot{b}_{a...b,E} F_{A...B}^{a...b} + b_{a...b,E} \dot{F}_{A...B}^{a...b}, \qquad (2.12)$$

which by the generalization of (1.4), is

$$\frac{d}{dt}(b_{a...b,e} F_{A...EE}^{a...be}) = \dot{b}_{a...b,e} F_{A...EE}^{a...be} + b_{a...b,e} \dot{F}_{A...EE}^{a...b} F_{E}^{e} . \qquad (2.13)$$

The result (2.11) follows by the obvious sequence of steps.

REFERENCES

- [1] Passman, S. L.: Convection-diffusion theorems. U. S. Naval Academy, Engineering Department Report 69-2 (1969).
- [2] Truesdell, C. A. and R. A. Toupin: The Classical Field Theories. Handbuch der Physik <u>III/1</u>, Berlin (1960).
- [3] Ericksen, J. L.: Tensor Fields. Appendix to [2].
- [4] Passman, S. L.: Two theorems in classical vorticity theory. Forthcoming.

Security Classification	THE STREET WHILE STREET WHILE STREET WHITE STREET
	NTROL DATA - R. & D ind annotation wast be artesed when the overall report is classified;
1. ORIG. ATING ACTIVITY (Companie subjet)	ing emission must be eristed when the aritall report is (lassified)
ENGINEERING DEPARTMENT	UNCLASSIFIED
UNITED STATES NAVAL ACADEMY	18. CROUP
ANNAPOLIS, MAKYLAND	
3. REPORT TITLE	
A COMMENTAL TO ACCUMENT	***************************************
A COMMUTATION FORMULA IN CONTINU	JUN MECHARICS
4. DESCRIPTIVE NOTES (Type of report and inclusive dates)	
an manantin too m the tree follow or reloct authoritative dates?	•
5. AUTHORISI (First name, miedie initiel, izat name)	
STEPHEN L. PASSMAN	
MEPONT DATE	78. TOTAL NO. OF PAGES 78. NO. OF KEFS
JULY 1969 SE CONTRACT OR SEANT NO.	16 4
*** ********* ** *********************	14. ORIGINATOR'S REPORT NUMBERIS)
& PROJECT NO.	E = 69 = 3
-	2 - 0/, - 3
* ·	19. OTHER REPORT HOLD (Any other numbers that may be existined this report)
	7
THE THE THE STATEMENT	-
Distribution of this document is	unlimited.
	*
II. SUPPLEMENTANY HOTES	12. SPONSORING MILITARY ACTIVITY
,	
D. ABBIRACT	
•	•
A plausibility argument is	given for the existence of a .
- certain commutation formula is g	given. This formula is then used
to derive a general type or conv	fection - diffusion theorem which.
generalizes a classical formula	TH KTHEMSCICST AGLEICITA LUGGLA.
•	
	•
•	
	•
•	
· .	
· · ·	
PAGE 1)	
OD FORM (PAGE I) S/II 0101-807-8811	NONE Security Crassification

KEY WORDS	LIN	K A	LIN	K B	LIN	. C
NET HORDS	ROLE	₩1	HOLE	w t	AGLL	7 W
Convection						
Diffusion						
Fluid Mechanics	1					
Continuum Mechanics						
Circulation						
Vorticity						
•			1			
			1			
				l .		
•						İ
•						
•	. -	1				
· .				Ì		
						İ
•						
·						
					1	
					ļ	
						•
•	,	1	1			
; \$~;	1					
•				ļ		
	·			i		
•		ĺ		i		

DD FORM 1473 (BACK)

Security Classification

NONE